

TITLE OF THE INVENTION

NUCLEAR MEDICAL DIAGNOSTIC APPARATUS

CROSS-REFERENCE TO RELATED APPLICATION

5 This application is based upon and claims the
benefit of priority from the prior Japanese Patent
Application No. 11-063884, filed March 10, 1999; and
No. 2000-57522, filed March 2, 2000, the entire
contents of which are incorporated herein by reference.

BACKGROUND OF THE INVENTION

10 The present invention relates to a nuclear medical
diagnostic apparatus for externally detecting gamma
rays emitted from RI (Radio-Isotope) injected to a
subject and generating an RI distribution in the
subject on the basis of the detection data.

15 Nuclear medical diagnostic apparatuses are
classified into planar image-type apparatuses which
obtain an RI distribution on a projection plane and
ECT-type (Emission Computed Tomography-type)
apparatuses which obtain an RI distribution on a slice.

20 The ECT type nuclear medical diagnostic apparatuses
include a SPECT (Single Photon Emission Computed
Tomography) apparatus using single photon RI such as
99mTc or 111In, and a PET (Positron Emission computed
Tomography) apparatus using positron RI such as 11C or
25 13N. Recently, apparatuses serving as both SPECT
apparatuses and PET apparatuses have appeared. These
apparatuses in general will be called nuclear medical

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position of an energy which does not coincide either of
the two positions P1 and P2 or naturally the true
incidence position. In other words, all the events
wherein scattering occurs in the scintillator are
5 counted as having occurred at erroneous positions. In
addition, conventionally, whether scattering occurs in
the scintillator cannot be determined.

In a PET-exclusive apparatus having a BGO (bismuth
germanium oxide) detector for performing block
10 detection as well, when gamma rays are scattered among
blocks of the BGO detector, the PET-exclusive apparatus
cannot separate events that occur simultaneously to
obtain the accurate positions of the events by
calculation. Accordingly, a decrease in counting
15 precision cannot be avoided.

BRIEF SUMMARY OF THE INVENTION

It is an object of the present invention to
decrease, in a nuclear medical diagnostic apparatus,
the probability of an incidence position detection
20 error derived from scattering in a radiation detector.

The radiation detector has a plurality of
semiconductor cells arrayed in a matrix. Each of the
plurality of semiconductor cells detects radiation
separately, and outputs a signal representing the
25 energy of radiation separately. A selection circuit
selects, among events wherein radiation is detected,
specific events wherein radiation derived from

radio-isotope injected to a subject is detected. In the first case wherein either one of the semiconductor cells outputs a signal, the energy of the signal is compared with a predetermined energy window. In the second case wherein two or more semiconductor cells output two or more signals substantially simultaneously, the total energy of the two or more signals is compared with the predetermined energy window. A position calculation circuit calculates, in the first case, the incidence position of radiation on the basis of the position of the semiconductor cell that outputs a signal, and in the second case, the incidence position of radiation on the basis of the position of either one of the two or more semiconductor cells. A counting circuit counts the specific events in association with the calculated incidence position. The distribution of radio-isotope in the subject is obtained on the basis of this counting result.

Additional objects and advantages of the invention will be set forth in the description which follows, and in part will be obvious from the description, or may be learned by practice of the invention. The objects and advantages of the invention may be realized and obtained by means of the instrumentalities and combinations particularly pointed out hereinafter.

BRIEF DESCRIPTION OF THE SEVERAL VIEWS OF THE DRAWING

The accompanying drawings, which are incorporated

in and constitute a part of the specification,
illustrate presently preferred embodiments of the
invention, and together with the general description
given above and the detailed description of the

5 preferred embodiments given below, serve to explain the
principles of the invention.

FIG. 1 is a sectional view of a conventional Anger
type gamma camera;

FIG. 2 is a view showing the frequency
10 distribution of the Compton scattering angle with
respect to the energy of the incidence gamma rays;

FIG. 3 is a graph showing the relationship between
an incidence energy and the energy of scattered rays at
various scattering angles;

15 FIG. 4 is a schematic sectional view of a
radiation detector used in a nuclear medical diagnostic
apparatus according to an embodiment of the present
invention;

FIG. 5 is a block diagram showing the arrangement
20 of the nuclear medical diagnostic apparatus having the
radiation detector shown in FIG. 4;

FIG. 6 is a view showing two positions where an
energy caused by one scattering event in semiconductor
cells is absorbed according to this embodiment;

25 FIG. 7 is a view showing three positions where an
energy caused by two scattering events in the
semiconductor cells is absorbed according to this

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the axis of ordinate represents the energy (E2) of the Compton scattered ray. From FIG. 3, it is obvious that when the incidence energy is 511 keV, that is, when these gamma rays are generated by positron, the energy E2 of the scattered ray falls within a range:

$$170 \text{ keV } (\theta = 180^\circ) \leq E2 < 511 \text{ keV } (\theta = 0^\circ)$$

When the scattering energy E2 falls within a range:

$$170 \text{ keV} \leq E2 < 255 \text{ keV } (511 \text{ keV} \times 1/2)$$

then a scattering angle θ falls within a range

$$75^\circ \leq \theta < 180^\circ$$

It is accordingly understood that 15% (painted portion in FIG. 2) of all the scattering events represents events having a scattering angle θ which falls within the range of $75^\circ \leq \theta < 180^\circ$. More specifically, it is concluded that, when gamma rays having an energy of 511 keV are scattered in the radiation detector only once, 85% of its scattering energy E2 is 256 keV (1/2 of 511 keV) or more. In other words, of the two energy absorption positions, the position where less energy is absorbed is determined as the scattering position (incidence position) with a probability of 85%.

This probability varies depending on the thickness and shape of the radiation detector. Simulation such as Monte Carlo simulation is performed in which the thickness and shape of the radiation detector are initialized. Through this simulation, the detection

surface can be divided into areas having a high probability that the position with a less energy is the incidence position, and areas having a high probability that the position with a larger energy is the incidence position. Therefore, the first rule according to which the position with the less energy is selected as the incidence position, and the second rule according to which the position with the larger energy is selected as the incidence position, can also be selectively employed in units of areas.

When this determination method is employed, according to the present invention, $1/2$ or more of the scattering events can be counted as having occurred at the true incidence positions, whereas the conventional Anger type gamma camera counts all the scattering events as having occurred at erroneously detected positions.

According to another method of reducing the probability of an incidence position detection error, when scattering occurs in a detector, i.e., when two or more semiconductor cells of one detector output signals substantially simultaneously, this event is excluded from the counting target. With this method, although the counting efficiency decreases more or less, the position detection error ratio can be suppressed to almost zero.

FIG. 4 is a schematic sectional view of a

semiconductor type radiation detector used in a nuclear medical diagnostic apparatus according to a preferable embodiment of the present invention. The radiation detector has a collimator 10, semiconductor cell array 20, and detection processing circuit 21. The semiconductor cell array 20 is formed on the rear surface of the collimator 10. The detection processing circuit 21 is formed on the rear surface of the semiconductor cell array 20. The semiconductor cell array 20 has a plurality of semiconductor cells 22 arranged in a matrix. The detection processing circuit 21 has a plurality of pre-amplifiers 23. The plurality of pre-amplifiers 23 respectively correspond to the plurality of semiconductor cells 22. The pairs of semiconductor cells 22 and pre-amplifiers 23 can detect radiation separately and output signals representing the energy of radiation separately. When the nuclear medical diagnostic apparatus is a coincidence PET apparatus, no collimator 10 is mounted on it.

The semiconductor cells 22 are made of, e.g., cadmium telluride (CdTe) or cadmium zinc telluride (CdZnTe). In place of the semiconductor cell array 20, a scintillation sensor formed by combining a scintillator (e.g., sodium iodide (NaI), LSO (Lutetium oxyorthosilicate), BGO (bismuth germanium oxide), and cesium iodide (CsI)) and a photoelectric conversion element (e.g., a photodiode) can be provided.

FIG. 5 is a block diagram showing the arrangement of the nuclear medical diagnostic apparatus having two opposing radiation detectors each shown in FIG. 4. The nuclear medical diagnostic apparatus shown in FIG. 5 according to this embodiment serves as both a single photon emission computed tomography (SPECT) apparatus and a coincidence positron emission computed tomography (PET) apparatus. The present invention can be applied to any one of a gamma camera, an SPECT apparatus, and a PET apparatus which generate an RI distribution (planar image) on a projection plane.

Two radiation detectors 50 and 51 are arranged to oppose each other through a subject. One radiation detector 50 has a semiconductor cell array 20 and detection processing circuit 21. The other radiation detector 51 also has a semiconductor cell array 30 and detection processing circuit 31.

Output signals (signals representing energies) from the detection processing circuits 21 and 31 are supplied to a signal processing circuit 40. The signal processing circuit 40 selects, among all the events wherein gamma rays are detected, a specific event (target event) wherein gamma rays derived from radio-isotope injected to the subject are detected is selected.

More specifically, in the first case, a signal is output from either one semiconductor cell 22 of each of

the radiation detectors 50 and 51. In this case, the energy of the signal is compared with a predetermined energy window. When the signal energy falls within the predetermined energy window, this event is counted as a target event in association with the incidence position or incidence path.

In the second case, two or more signals are output from two or more semiconductor cells 22 of one of the radiation detectors 50 and 51 because of the Compton scattering or the like (internal coincidence event). In this case, the energies of the two or more signals output from the radiation detector 50 or 51 substantially simultaneously are added, and their total energy is compared with the energy window. When the signal energy falls within the predetermined energy window, this event is counted as a target event in association with the incidence position or incidence path.

An internal coincidence circuit 46 calculates the time differences between the signal output from either one of the plurality of semiconductor cells 22 of one of the radiation detectors 50 and 51 and the signals output from the remaining semiconductor cells 22, and compares each time difference with a predetermined threshold. When the time difference is smaller than the predetermined threshold, the internal coincidence circuit 46 determines that this event falls under the

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output from the detection processing circuits 21 and 31 in PET counting is equal to or less than a predetermined threshold, an external coincidence circuit 42 checks whether an event wherein gamma rays are detected is a coincidence event (external coincidence event) wherein gamma rays derived from radio-isotope injected to a subject are detected. If so, the external coincidence circuit 42 outputs a signal representing an external coincidence event to the signal processing circuit 40. The signal processing circuit 40 counts this external coincidence event in association with an incidence path.

An incidence path calculating circuit 44 calculates a straight line connecting the incidence position of one radiation detector 50 and the incidence position of the other radiation detector 51, both of which have been calculated by the incidence position calculating circuit 43 during PET radiography, as the incidence path of the gamma rays. A displaying unit 45 displays a SPECT image or PET image obtained by image reconstruction of the image reconstructing circuit 41.

FIG. 6 shows the second case wherein the gamma rays are scattered in the semiconductor cells 22 of the radiation detector 50 or 51 and their energy is absorbed at two points P1 and P2. In this case, signals are respectively output from semiconductor cells 22 corresponding to the positions P1 and P2

5 The energy window described above can change
depending on positions. In this case, the precision of
the calculated incidence position can be improved
remarkably. For example, the photoelectric absorption
probability of 511-keV positron nuclide of a
10 semiconductor cell, at a portion having a thickness of
about 10 mm, made of cadmium telluride (CdTe) or
cadmium zinc telluride (CdZnTe) described above is
about 7.4%, and its scattering probability is about
28.5%. A probability that the energy of gamma rays
15 which have been scattered once is absorbed in the
semiconductor cell array 20 is present with a
proportion unnegligible when compared to the
photoelectric absorption probability described above.
Therefore, if the calculating method described above is
20 employed, the same effect as the equivalent improvement
of the detection sensitivity (improvement of the count)
can be obtained, when compared to a case wherein all
the incidence positions of the gamma rays are
erroneously calculated in an Anger type gamma camera.
25 (Position Calculation)

In the first case, the gamma ray incidence position is calculated on the basis of the position of

one semiconductor cell 22 that has output the signal. More specifically, the central position of one semiconductor cell 22 that has output the signal is calculated as the gamma ray incidence position.

5 In the second case, the gamma ray incidence position is calculated on the basis of the position of either one semiconductor cell 22 among two or more semiconductor cells 22 that have output the signals substantially simultaneously. More specifically, the
10 central position of the semiconductor cell 22, among the plurality of semiconductor cells 22 that have output signals, that has output a signal having the lowest energy is calculated as the gamma ray incidence position. According to this rule, the true incidence
15 position can be obtained with a probability much higher than 50%, as described above.

 According to another rule, calculation may be performed in the following manner. When the plurality of semiconductor cells 22 that have output signals
20 substantially simultaneously are located in the first area of the detection surface, the central position of the semiconductor cell 22, among these semiconductor cells 22, that has output a signal having the lowest energy is calculated as the gamma ray incidence
25 position. When the plurality of semiconductor cells 22 that have output signals substantially simultaneously are located in the second area of the detection surface,

the central position of the semiconductor cell 22, among these semiconductor cells, that has output a signal having the highest energy is calculated as the gamma ray incidence position.

5 During coincidence counting, when gamma rays (gamma rays derived from positron) coming incident on the semiconductor cell array 30 in the radiation detector 51 are scattered and absorbed once, the gamma ray incidence position is calculated in accordance with the same calculation scheme as that described above.

10 FIG. 7 shows a case wherein gamma rays are scattered at two positions. In this case, the energy is absorbed at three positions P1, P2, and P3. Namely, three semiconductor cells 22 output signals
15 substantially simultaneously. The three signals respectively represent energies E1, E2, and E3 (keV).
(Event Selection)

20 The signal processing circuit 40 adds the energies E1, E2, and E3, and compares their total energy (E1 + E2 + E3) with a predetermined energy window. The signal processing circuit 40 then checks whether the total energy (E1 + E2 + E3) satisfies a relationship:

$$E_c - W < E_1 + E_2 + E_3 < E_c + W$$

25 If this relationship is not satisfied, this event is excluded from the counting target. If this relationship is satisfied, this event is counted as a target event in association with the incidence position

Assume that the gamma rays that are scattered the second time have the maximum energy. In the first scattering, forward scattering is dominant. If the detection positions of the two energies absorbed after first and last scattering are simply averaged, an incidence position more accurate in average than that obtained by weighted addition of the respective energies generated in an Anger type gamma camera can be obtained.

Assume that the gamma rays that are scattered the third time have the maximum energy. In two initial scattering cycles, forward scattering is dominant, and the range of the second scattering is long. Hence, when the detection positions of the two energies absorbed after two initial scattering cycles are simply averaged, the precision of the incidence position is largely improved.

As shown in FIG. 7, the probability that scattering occurs twice is much smaller than the probability that scattering occurs once. Yet, this can improve the precision of the calculated incidence position more than in the case using the Anger type gamma camera. In this manner, the calculation process of the incidence position as shown in FIGS. 6 and 7 can be applied to gamma rays which can cause forward scattering with a high probability (i.e., to gamma rays having a comparatively high energy).

Above explanation refers to calculation of the incidence position of gamma rays when relatively small energies are detected at two detection positions. When relatively small energies are detected at three or more detection positions, the barycenter of these detection positions may be calculated, and their barycentric position as the calculation result may be determined as the gamma ray incidence position.

FIG. 8 is a view showing the schematic arrangement of a gamma camera as a nuclear medical diagnostic apparatus having two opposing detectors (an apparatus in which radiation detectors are arranged to oppose each other through a subject) according to the embodiment of the present invention, and explains a positron imaging method using this gamma camera.

FIG. 8 is based on the following assumption. One gamma ray generated by positron Po comes incident on the radiation detector 50, is scattered once, and is then absorbed. The other gamma ray comes incident on the radiation detector 51 and is back-scattered at a scattering angle of θ . After that, backscattered gamma rays concerning the remaining energy come incident on the radiation detector 50 entirely and are absorbed. A gamma ray incidence path is calculated on this assumption. More specifically, FIG. 8 shows a case wherein three events occur in the radiation detector 50 simultaneously, whereas one event occurs in the

radiation detector 51.

To perform coincidence counting, outputs (trigger signals) from positron generation time detection circuits (not shown) in the detection processing

5 circuits 21 and 31 respectively formed in the two

radiation detectors 50 and 51 that oppose each other

through the subject P are output to the coincidence

circuit 42. Based on these trigger signals, the

10 coincidence circuit 42 checks whether energies E2, E3, and E4 of the gamma rays absorbed in the radiation

detector 50 and an energy E1 of the gamma rays absorbed

in the radiation detector 51 are related to the gamma

rays generated by positron Po simultaneously.

15 If these energies are not recognized to be related to the gamma rays coming incident on the radiation

detectors 50 and 51 simultaneously (if they are not

recognized as coincidence counting), information on

these energies should not contribute to positron

imaging. If these energies are recognized to be

20 related to the gamma rays coming incident on the radiation detectors 50 and 51 simultaneously, the

incidence position calculating circuit 43 performs the

following process in response to this recognition

result on the basis of the energy signals and position

25 signals output from the detection processing circuits

21 and 31.

First, assume that backscattering occurs in the

radiation detector 51 and consequently backscattering gamma rays BS come incident on the radiation detector 50, as shown in FIG. 8. A scattering angle θ of the gamma rays BS falls within the range of $90^\circ \leq \theta \leq 180^\circ$, and 90° scattering corresponds to about 220 keV.

Accordingly, on the basis of the energy E_1 absorbed in the radiation detector 51, whether a relationship $220 < E_1 < 511 - W$ (keV) or $E_1 < 170$ (keV) is satisfied is checked. Note that W is the window in interest, as described above.

If the relationship $220 < E_1 < 511 - W$ (keV) or $E_1 < 170$ (keV) is satisfied, information on the energy E_1 should not contribute to imaging. If the energy E_1 falls within the range of $170 \leq E_1 \leq 220$, the energy E_1 is added with each of the energies (E_2 , E_3 , and E_4). Namely, $E_1 + E_2$, $E_1 + E_3$, and $E_1 + E_4$ are calculated to acquire sums E_1 , E_2 , and E_3 .

It is checked whether each sum satisfies a relationship E_1 (E_2 or E_3) $< 511 - W$ (keV) or E_1 (E_2 or E_3) $> 511 + W$ (keV). If any sum satisfies either relationship, information on these energies should not contribute to imaging.

If a sum that satisfies a relationship $511 - W \leq E_1$ (E_2 , or E_3) $\leq 511 + W$ (keV) exists, a position (x_1 , y_1) in the radiation detector 51 where the energy E_1 is detected is determined as the incidence position of the gamma rays derived from positron. In this case, the

sum $E1 = E1 + E2$ satisfies the relationship $511 - W \leq E1 \leq 511 + W$ (keV).

The energy $E2$ used for determination of the gamma ray incidence position in the radiation detector 51 is excluded from the energies $E2$, $E3$, and $E4$ detected in the radiation detector 50, and two remaining energies $E3$ and $E4$ are added to acquire a sum $E4$.

On the basis of the sum $E4$, whether $E4$ satisfies the relationship $E4 < 511 - W$ or $E4 > 511 + W$ is checked. If the sum $E4$ satisfies this relationship, on the same principle as that of the case shown in FIG. 6, the position where a lower energy, of the two energies $E3$ and $E4$ that are added, is detected is determined as the incidence position where the gamma rays derived from positron come incident on the radiation detector 50. Then, the incidence path of the gamma rays derived from positron is calculated on the basis of the incidence positions on the radiation detectors 50 and 51.

The present invention is not limited to a case wherein three incidence events occur in the radiation detector 50. When two, or four or more incidence events occur, the same method as that described above can be used.

FIG. 9 explains a case wherein absorption correction of gamma rays is performed by utilizing backscattered rays, without using a special gamma ray

absorption correction ray source, on the basis of the method described by using the gamma camera shown in FIG. 8. In FIG. 9, when backscattering is caused in two radiation detectors 50 and 51 opposing each other through a subject P as shown in FIG. 8, backscattered rays BS1 and BS2 come incident on the other radiation detectors 51 and 50, respectively. In this case, the energy values of these backscattered rays can be estimated with a certain fluctuation. Hence, these backscattered rays can be supposed to be the gamma ray absorption correction ray source having these energies.

More specifically, when acquiring ordinary coincidence counting PET, in addition to utilizing the backscattered rays BS1 and BS2 as described above, if the energy distributions of the backscattered rays at a certain detection position of the gamma rays at respective angles in the radiation detectors 50 and 51, and their frequencies are estimated from a certain typical patient model, gamma ray absorption correction data can be simply formed by using this estimation. By employing this method, absorption correction of the gamma rays can be performed without specially forming absorption correction data by using a gamma ray absorption correction ray source.

The method described with reference to FIGS. 8 and 9 is not limited to a case wherein the gamma camera described above, which has two opposing detectors, is

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5 Additional advantages and modifications will
readily occur to those skilled in the art. Therefore,
the invention in its broader aspects is not limited to
the specific details and representative embodiments
shown and described herein. Accordingly, various
10 modifications may be made without departing from the
spirit or scope of the general inventive concept as
defined by the appended claims and their equivalents.